Strategic planning of North Atlantic Oceanic air traffic based on a new wind-optimal route structure

I. INTRODUCTION

The North Atlantic airspace (NAT) accommodates air traffic between Europe and North America. It is considered as the second largest oceanic airspace, after the Pacific airspace, and it is the busiest one in the world. In 2012 about 460,000 flights crossed this airspace [2]. Due to increasing passenger demand, time zone differences, jet streams, this vast airspace becomes very congested, especially in peak hours, namely between 1200-1800 Coordinated Universal Time (UTC) for westbound traffic and between 0100-0600 UTC for eastbound one. Currently, the major tool of surveillance applied on the oceanic airspaces is the High Frequency voice Positions (HF-POSs) according to which aircraft have to communicate to the Oceanic Area Control Center (OACC), their positions and specific data. However, poor propagation conditions and communication equipment failures often downgrade this communication. Therefore, controllers prefer rather to apply strategic traffic planning in order to overcome the surveillance difficulties. Besides, aircraft operating on the NAT airspace are subject to very strong winds due to the jet streams. These streams are fast flowing air currents running mainly from west to east. They typically run between 20,000 and 50,000 feet with a speed around 100kts and can reach 200kts. Their width is relatively narrow compared to their length. As a result, air traffic in the NAT airspace is divided into two major flows: the westbound flow travels from Europe to North America in the morning and eastbound flow travels in the opposite direction in the evening. Normally, eastbound flights exploit the jet streams in order to benefit from strong tailwind, while westbound flights would rather avoid the jet streams and stay away from headwinds. In order to overcome all these constraints, namely the lack of surveillance and jet streams, a structure of routes, called Organized Track System (OTS), was established in the North Atlantic airspace. These routes are daily constructed to satisfy as much as possible the optimal flight profiles. Besides, aircraft are required to apply very restrictive separation standards. Currently, the oceanic norms of separation are higher than the continental one because of the lack of radar coverage over oceanic area. These very demanding separation standards limit the efficiency of the oceanic airspace. Considering these issues, a new kind of communication system, called Automatic Dependence Surveillance-Broadcast (ADS-B), has been recently introduced. Thanks to the accuracy of this system, the oceanic standard separation will be relaxed. Currently, ADS-B systems use is increasing around the world. For instance, applying the ADS-B is becoming mandatory for all aircraft operating on the European, Canadian and Australian airspaces since 2015. Moreover, the US has near-term plans to mandate its deployment by 2020 [17]. Besides, statistics showed that, by 2020, 95% of aircraft operating on the NAT airspace will be equipped with ADS-B systems (or equivalent) [2]. Therefore, supposing that all aircraft are equipped with ADS-B is a conceivable assumption which can turn to a fact in the near future.

Our objective, in this work, is to substitute the OTS system while ensuring an optimal management of the traffic. The main idea is to take advantage from both the application of ADS-B systems, and the exploitation of the jet streams in order to construct wind optimal routes. Thus, we consider only eastbound flights that can benefit from the jet streams. In fact, several researches showed that travelling wind optimal routes have a great positive effect on fuel consumption. For this reason, we propose to merge the OTS tracks on the jet streams. At the same time, we suppose that all aircraft are equipped with ADS-B system so that we can profit from a significant reduction on the separation standards. The most
important gain, to be reached by applying this new structure of routes, is to put as many flights as possible on the jet. Therefore, these flights can follow near wind-optimal routes. Thus, we propose, in this paper, a new structure of routes over the NAT airspace that takes advantages from the jet streams. Then, we propose a method to optimize the strategic flight planning using this oceanic route structure. The rest of this paper is organized as follows: The next section describes the actual route structure on the NAT airspace. Section III contains relevant works on optimizing air traffic over the oceanic airspace. Section IV presents the problem formulation. We mainly describe the new developed route structure and present the flight model that we adopt. We expose also the wind networking model. Section V exposes the methodology of conflict detection and resolution. Computational results are presented in section VI. Finally, we conclude in section VII.

II. BACKGROUND

In this section, we present a theoretical background related to our research topic. First, we describe the OTS routes, which represents the actual route structure in the NAT airspace. Then, we introduce a brief description of the ADS-B system and we expose the potential benefits behind its deployment.

A. The Organized Track System

In order to ensure safe flights over the NAT airspace, the OTS system is established. It is a set of trans-atlantic flight routes that links the Northeast of America to Western Europe. OTS includes typically from 5 to 7 parallel or nearly parallel tracks in each direction (eastbound and westbound) between the altitudes of 29,000 and 41,000 feet. Around 10 waypoints are planned in each track. The tracks are constructed, daily, to take into account the shifting of west-east jet streams. Aircraft operating over the NAT airspace have to satisfy vertical, lateral and longitudinal separation. The OTS system is constructed to satisfy these separation norms. Indeed, the tracks are separated by 60NM laterally and 1000 feet vertically (the actual separation norms). Thus, once the aircraft are on the OTS route structure, controllers have only to ensure the longitudinal separation between them. In fact, the longitudinal separation is calculated in terms of time and represents the time between two consecutive flights following the same track. Thus, the longitudinal separation is 10 minutes between two consecutive aircraft following the same track. If an aircraft changes its track, the longitudinal separation becomes 15 minutes with the flights in the new track (Figure 1). As illustrated in figure 2, the OTS can be represented by a grid of three axes $N_x$, $N_y$ and $N_z$:

- **Axe $N_x$**: Labelled from 1 to $N_x$ oriented to the east, it contains a set of nodes representing the waypoints in each track.
- **Axe $N_y$**: Labelled from 1 to $N_y$ oriented to the north, it represents the number of OTS tracks.
- **Axe $N_z$**: Labelled from 1 to $N_z$ started from the lowest.

Although there is no radar over the ocean, oceanic controllers must still make sure all the aircraft are conducted safely. Since they cannot see the aircraft, controllers rely on pilots to report their position at regular intervals. A position report provides an aircraft’s location, speed, and altitude. Pilots used to apply High Frequency Voice Positions to communicate their reports to oceanic control centers. Actually, on most occasions, when pilots communicate with Oceanic Air Traffic Control Centres (OATCC), they do not talk directly to controllers. An international flight service station (IFSS) is responsible to relay messages between aircraft and OATCC. Such units are not always co-located with an OATCC. Besides, it is important to note that controller workload is usually high. Thus some delays can be expected for responses to requests for a change of flight level, route, etc. Besides, we note that depending on atmospheric conditions, it can be relatively noisy with the signal in and out. For these reasons, oceanic controllers usually deny rerouting from one track to another inside the OTS [2]. Thus, flights are more likely to keep the same track from the entrance to the exit of the OTS, and re-routing is rarely authorized.

B. ADS-B systems

The availability of ADS-B represents an opportunity to enhance air traffic management over the NAT airspace. ADS-B is an airborne-based system that relies upon automatic
position reports in order to provide both pilots and controllers with more accurate and reliable information. Based on the principle of providing a global coverage, the ADS-B system ensures a periodic transmission of the aircraft information (position, velocity and heading), via a broadcast data link, to both the controllers and the surrounding traffic. Thanks to the accuracy of this surveillance tool, the air traffic situation will be improved in the oceanic airspace. Thus, a significant reduction in the separation norms can be applied. Longitudinal separation between two aircraft in the same track becomes 2 minutes, instead of 10 minutes when the two aircraft are consecutive on the same track, and 3 minutes instead of 15 minutes, if an aircraft changes its track. Further informations and details about the functionalities of ADS-B systems are given in [3], [1]

III. RELATED WORK

In the literature, several works deal with the problem of improving aircraft situation over the oceanic airspace. They focus on optimizing flight routes by re-routing the aircraft inside the OTS structure. Each flight is represented by several parameters, such as entry and exit tracks, flight level and Mach number. Once inside the OTS tracks, a flight can request to change some of its parameters. This change can be a re-routing from the initial track, switching to another flight level or varying the Mach number. In [12], authors assumed that all aircraft are equipped with ADS-B systems. Thus, the reduced separation standards can be applied. Under these conditions, aircraft can regularly change tracks. OTS structure is represented by a grid of nodes and links. Each aircraft has the possibility to change its track only on nodes by moving one track up or down. The Genetic Algorithm (GA) is applied to find the optimal flight paths while avoiding conflicts. The same authors applied the Simulated Annealing algorithm (SA) with the same model to resolve the same trajectory optimization problem in [14]. The application of the two algorithms shows that operating the ADS-B system can remarkably improve the traffic situation. Besides, both algorithms can reach a conflict-free solution for real traffic data while optimizing a specific objective function. However, the SA algorithm gets better solutions than the GA algorithm for the considered problem, in much less time. Another work [4] aims to optimize the NAT air traffic by removing the OTS structure and using nearly direct flight routes instead. The idea is to apply the flocking boid model in order to construct a full swarm behavior while assuming that all aircraft are equipped with ADS-B systems. The flight trajectories are represented as a set of discrete points. Initially, each flight heading is steered to its destination point. Then, in each time sample, the flight heading is adjusted using the boid flocking model. Actually, the flocking model represents the form of collective behavior of a large number of interacting agents. It relies upon three heuristic rules. First, the separation rule which guarantees a separation distance between agents, hence, it permits to avoid conflicts. Second, the cohesion rule which is used to ensure the swarm behavior. Finally, the alignment rule which is used in order to maintain agent trajectories quasi-parallel. Besides, considering the specificities of the problem, two additional rules have been included, namely, a force to oblige the flight to reach its destination and a force to avoid the oscillation of the trajectories. The SA algorithm is applied in order to find the optimal balance between the different forces in each time sample. The computational results prove a considerable reduction in the number of conflicts with reasonable delay and elongation from the direct path. Besides, several works consider the aircraft trajectories optimization problem in presence of wind in both continental and oceanic airspace. [5], [11] focus on air traffic optimization in the continental airspace. Concerning the oceanic airspace, many studies treat the NAT airspace. Typically, they consider only eastbound traffic in order to exploit the jet stream tail-winds. [16] evaluate the potential benefits from flying wind-optimal routes in the NAT airspace. It shows that a significant gain can be reached when aircraft follow wind-optimal paths regarding cruising time and fuel saving. Another study [10] developed an algorithm that optimizes Trans-Atlantic flight trajectories in presence of winds. The process is divided into two stages. First, the optimal vertical profile for each aircraft is calculated. Then, optimal aircraft headings considering the wind on multiple flight levels are determined. As for the previous study, simulation results allow to conclude that traveling wind-optimal trajectories with optimal vertical profile save time and fuel. However, these wind-optimal routes generate a large number of potential conflicts between flights. In fact, for the two aforementioned works, the conflict detection and resolution problem is not considered. They focus only on optimizing one flight trajectory without considering the totality of the traffic. Some recent works aim to de-conflict wind-optimal routes over the oceanic airspace. For instance, both studies [15], [13] introduce strategic methods that detect and resolve conflict of wind-optimal flight trajectories in the NAT airspace. In [15], de-conflicting wind-optimal routes were ensured with a SA algorithm combined with local gradient search. The potential number of conflicts was reduced by a small adjustment in departure times and rerouting. In [13], the conflict resolution is insured by a SA algorithm and is based on two maneuvers: changing the departure time, and slightly modifying the geometrical shape of the trajectory while remaining wind-optimal. Computational results show that an interesting reduction in the number of conflicts can be reached. Nevertheless, this method of wind-optimal trajectories is not robust regarding the change of meteorological conditions. In fact, when taking into account uncertainties in wind data, new conflicts appear and the proposed method does not provide solutions to this problem. Moreover, [6] represents the first study that discusses the potential benefit from traveling wind-optimal routes instead of using the Central East Pacific (CEP) airspace route structure. A backward recursion dynamic programming algorithm is used to calculate wind-optimal flight routes. The same
authors treat the problem of conflict detection and resolution of the wind-optimal routes in [7]. The idea is to strategically schedule flights while ensuring that the interaction between trajectories is manageable. The problem was modeled as a job shop scheduling issue. It has been solved via 0-1 integer programming model. Simulation results prove that the annual economic benefit for airlines companies range between $3.4 million and $8.5 million if flights follow wind-optimal routes on the CEP. However, it is obvious that flights which follow preferred routes and override the established route structure will never follow in practice the exact pre-determined paths and predicted conflicts may never happen. Therefore, a realistic solution to manage oceanic air traffic necessarily passes through a route structure.

In our study, we focus on the eastbound strategic flight planning. We combine two paradigm in order to benefit from the advantages and strengths of each one. First, we keep the route structure in order to overcome the surveillance coverage problem, leading to a more reliable and safe traffic over the NAT airspace. Second, we adjust the route structure to the jet streams direction in order to obtain approximate wind-optimal trajectories.

IV. PROBLEM FORMULATION

We consider a set of $N$ eastbound flights. Each flight is represented by a set of parameters which are:
- Entry and exit track,
- Track entry time,
- Flight level at waypoints,
- True airspeed in knots.

Some of these parameters have fixed values that will not change all along of the problem resolution, while the other values could be changed. These latters are the variables of our optimization problem. Indeed, we assume that the aircraft speed is constant for the entire trajectory. This assumption is conceivable since we are tackling only the en-route phase. On the other hand, its important to extend the state space in order to guarantee conflict-free trajectories. Thus, entry delay less than 20 minutes is allowed. Moreover, the entry and exit tracks can be relaxed by allowing aircraft to enter and/or exit an adjacent track. Actually, we mainly do not prefer to change the vertical profile of the aircraft, since it guarantees the optimal fuel-consumption. Nevertheless, we permit to change the requested flight level at waypoints as a last alternative when no conflict-free solution exists. This modification of flight level is restricted to aircraft climb.

Descent is not allowed. Besides, changing the entry/exit flight level are not allowed in order to meet as much as possible airline companies preferences. The entry data of our model are represented below:
- $Track_{in} \in 1,2,\ldots,N_y$ the desired entry track
- $Track_{out} \in 1,2,\ldots,N_y$ the desired exit track
- $T_{in}$ the entry time
- $FL_i \in 1,2,\ldots,N_z$ where $i \in 1,2,\ldots,N_y$, the flight level at each waypoint expressed in feet. The distance between each two consecutive flight level is equal to 10 feet.

In order to represent the relaxation that we allow in some flight’s parameters, we define the following decision variables:
- $ATrack_{in} = Track_{in} + / - 1$ the assigned entry track.
- $ATrack_{out} = Track_{out} + / - 1$ the assigned exit track.
- $D_{in} \in [0, 20\text{min}]$ the time delay at the entry point.
- $Z_i$ where $i = 1, 2, \ldots, N_y - 1$ binary parameter characterizing the flight altitude profile $Z_i = (FL_i - FL_{i-1})/10 = \begin{cases} 
1 & \text{if the flight climbs to the next level at waypoint } i \\
0 & \text{otherwise} 
\end{cases}$ with $(Z_1 = 0)$.

Towards ensuring conflict-free trajectory for each aircraft, we assign different values for the parameters of each flight. These values remain close to the initial values.

In addition, another important goal is to benefit from wind-optimal routes. Therefore, we opted to benefit from the jet streams by using wind-optimal routes structure instead of OTS routes.

V. PROPOSED NEW ROUTE STRUCTURE

In this section, we propose a new route structure over the NAT airspace which benefits from jet streams. Two major factors influenced the construction of this new structure. First, it is obvious that en-route fuel consumption is strongly influenced by weather conditions, such as wind speed and direction. For this reason, we put the eastbound flights in jet streams direction. The second important factor is that, as mentioned previously, we consider the hypothesis that all aircraft implement the ADS-B system. Therefore, our proposed structure benefits from the reduction of separation norms.

A. Route structure

As we have seen, in the OTS structure, tracks are separated by 60 NM, while, in our new structure, we keep tracks separated by 10 NM. This reduction is reasonable since we are interested in aircraft equipped with ADS-B system. Our new structure of routes is described as follow:

We keep the same entry and exit points of the OTS tracks. Beginning from the first points of each track, we merge all tracks to the center where we have jet streams. Then, we keep tracks parallel and separated by 10 NM along 1000 NM. Finally, each track joins the corresponding exit point of the OTS system (Figure 3). Besides, in the portion of our structure where tracks are separated by 10 NM, we do not allow aircraft to change their track. Indeed, an aircraft entering in the parallel track section has to keep its track up to the exit point of this section. Obviously, flights crossing the OTS track system do not keep the same track from the entering to the exit point. For this reason, our structure has to satisfy this constraint and guarantee reliable transition between the rails. Thus, sections before and after the parallel track region are considered as filters. In these sections each track contains waypoints. Flights are allowed to change their tracks only on these waypoints. Besides, maintaining the
preferred flights altitude profile is recommended since it guarantees optimal fuel consumption. Thus, even though we forbid transitions from one track to another inside the parallel track region, aircraft can change their flight levels according to their preferred altitude profiles over this region. For this reason, three waypoints per track are used only to change flight levels while maintaining the same track in the parallel region. Therefore, tracks are represented by a set of waypoints related by links. Flights crossing this route structure are only allowed to change their tracks on waypoints (in the filter regions). In each waypoint, the flight has three alternative maneuvers: whether it continues with the same track or it changes its track to an adjacent one (north or south).

B. Route structure model

We can model our route structure as following. Our structure can be represented as a grid with \( N_t \) tracks, each track contains \( N_w \) waypoints and \( N_z \) flight levels. Figure 4 illustrates the grid model in horizontal dimension. When an aircraft enters a predefined track at a predefined flight level, its required to follow the same track and flight level unless a maneuver is done. This maneuver can only be held on waypoints. Thus, arriving to a waypoint, a flight has several possibilities to continue its path. It can rather change the flight level or pursue at the same altitude. Besides, when keeping the same flight level, it has also the possibility to change its track to an adjacent one. Thus, only one change is allowed at a given waypoint and changing at the same time the flight level and the track is forbidden. Thus, in addition to the decision variables introduced in the section IV, we introduce the following variables which permit to represent the eventual maneuvers over our new route structure: \( X_i \) where \( i = 1, 2, \ldots, N_t - 1 \) binary parameter defining the flight routing maneuvers

\[
X_i = \begin{cases} 
1 & \text{if the flight switches to the northern adjacent track at the waypoint } i \\
0 & \text{if the flight continues with the same track} \\
-1 & \text{if the flight switches to the southern adjacent track at the waypoint } i 
\end{cases}
\]

The \( X_i \) points represent the waypoints where a rerouting from one track to another is possible, precisely, the waypoints of the filter regions.

C. Wind networking

In order to be as close as possible from real oceanic traffic, it is important to consider the wind network in the simulation of flight’s progress. Actually, to simulate flight trajectory, we compute for each aircraft the time of passing the waypoints of the route structure. These times depend on two factors. On the one hand, it varies upon the aircraft true airspeed, which is a given data in our problem. On the other hand, the passing time depends on the wind direction and speed. Thus, considering our structure, we have to compute wind vector in both waypoints and links. To do so, we calculate the wind vector in each node of the route structure using a grid of wind data. Thus, for each node, we associate the east wind component \( W_E \) and the north wind component \( W_N \). Then, we deduce for each node the wind norm given by: \( \| \mathbf{W} \| = \sqrt{W_E^2 + W_N^2} \) and the associated wind bearing \( \theta_W = \arctan(W_E/W_N) \). Once we get the wind informations for each node, we can calculate the tail wind in each link. In deed, each link connects an origin node \( N_o \) and a destination one \( N_d \). Let \( (\phi_o, \lambda_o, z_o) \) and \( (\phi_d, \lambda_d, z_d) \) be respectively the spherical coordinates of the nodes \( N_o \) et \( N_d \). The associated bearing \( \theta_l \) of each link \( l \) is given by the following formula:

\[
\theta_l(N_o,N_d) = \arctan \left( \frac{\sin(\Delta\lambda).cos(\phi_d)}{\cos(\phi_o).\sin(\phi_d) - \sin(\phi_o).\cos(\phi_d).\cos(\Delta\lambda)} \right)
\]

where \( \Delta\lambda = \lambda_d - \lambda_o \). Based on the previous equation, we can calculate the tail wind on each extremities of the link \( TW_o \) and \( TW_d \):

\[
TW_o = \| \mathbf{W}_o \| .cos(\theta_l - \theta_W_o)
\]
\[
TW_d = \| \mathbf{W}_d \| .cos(\theta_l - \theta_W_d)
\]

Then, we associate to each link the average of those two tail wind :

\[
TW = \frac{TW_o + TW_d}{2}
\]

The time needed by the flight to reach node \( N_d \) from node \( N_o \) can be now deduced by :

\[
t = \frac{d_l}{T_u + TW}
\]

where \( d_l \) represents the great circle distance of the considered link and \( T_u \) is the true airspeed of the aircraft.
VI. CONFLICT DETECTION AND RESOLUTION

This section presents the methodology used to obtain conflict-free trajectories over the NAT airspace. First, we present our conflict detection approach. Then, we describe our conflict resolution algorithm including different ways used to remove conflicts.

A. Conflict detection strategy

In air traffic control, a conflict represents a violation of established separation norms. As previously mentioned, in our study, we consider oceanic separation norms assuming that all aircraft are equipped with ADS-B systems. For this purpose, we precisely build our route structure (detailed in V-B) based on these reduced separation norms (tracks are separated by 10 NM, flight levels are separated by 1000 ft). It only remains for us to manage the longitudinal separation which is assumed to be 2 minutes if aircraft are in the same track, and 3 minutes when an aircraft changes its track. Figure 5 shows the longitudinal separation norms. Besides, an aircraft has also the possibility to change its flight level (only by climbing). The aircraft position deviation in the horizontal plane is neglected, as well as the time required to reach the new flight level. However, when changing its flight level, an aircraft has to maintain a new separation norm with aircraft flying on the same track at the new flight level. The separation standards, in this case, become 2,2 minutes. Considering our route structure, we either detect a conflict at nodes or at links. At nodes level, conflicts are detected by sorting flights passing through a given node according to their transit time. Once sorted, we compute the difference in transit time between each two successive flights. A conflict is detected when this value is less than the longitudinal separation. Since each link is delimited by two nodes, we can detect conflict at links level by comparing the sequence order of aircraft at the entry and exit nodes of a link. If there are two swapped flights, then a catch up conflict is detected.

B. Optimization process

In this work, we seek for optimal flight trajectories by optimizing cruising time while remaining conflict-free and satisfying some constraints such as respecting a maximum delay per flight. To reach this goal, we start with pre-processing the flight set using a sliding window method (SW). The latter consists in dividing the problem into a set of sub-problems. Then, each sub-problem is treated separately and sequentially via a simulated annealing algorithm (SA). The SW method consists on sorting the flight set according to the entry time to the route structure. Then, a time window interval that begins at the earliest entry time and with a length $T_w$ is fixed. In each time window, four types of flight are defined. Planned flights are those that begin after the time window. Completed flights are those that have already finished their travel time before the time window. Besides, on-going flights are aircraft that begin before the time window and still operate in the considered time interval. Finally, active flights are those having entry time in the considered time window. Once we define the four flight types, we proceed with the de-confliction method. Planned and completed flights are not considered. We apply the SA algorithm to fix the decision variables (parameters) of the active flights while considering the on-going trajectories as constraints. Hence, the decision variables of on-going aircraft are not modified. In the next iteration, we shift the time window by $T_s$ (with $T_s < T_w$). This process is repeated until finally all flights are completed. Figure 6 illustrates a schematic example of the SW process. Once a time window is defined with the on-going flight fixed and the activate flight determined, we apply the SA algorithm. The latter is a meta-heuristic algorithm inspired from thermodynamics. Further details about this meta-heuristic are present in [8], [9]. SA aims to minimize an energy function. The concept consists in accepting change even to a worse situation, but in a controlled manner. The system begins with a random
solution and with a pre-determined control parameter $T$ (called temperature). The latter decreases as the number of iteration rises. At each step, SA calculates a neighboring solution. It associates to each solution an energy value and probabilistically decides to keep either the neighboring solution or the current one. When $T$ is large (the heating up step), exploration of the search space is promoted. However, when $T$ is small (cooling-down step), the system will converge towards the locally best solution. The SA algorithm is adapted to solve our problem as following:

- The search space consists of all possible set of flight trajectories. A solution is determined when we fix for each aircraft in the flight set the decision variables.
- The energy function is our optimization problem objective function, which we detail in the next section.
- A neighbor solution is obtained by applying a local change to the current solution. It consists of changing one decision variable of an aircraft inside the flight set.

The process of getting a neighbor solution is divided in two steps. First, we select the flight to be modified based on the following heuristic. We choose the flight that generates the biggest number of conflicts. Then, we select the decision variable. In order to satisfy as much as possible aircraft preferences, we consider a priority order when modifying flights parameters. Indeed, we give the biggest probability to the shifting of the en-route maneuver, since it does not affect much trajectory length. Then, we consider modifying the entry/exit tracks. If a conflict-free solution does not exist, we delay the flight entry time. The last maneuver is to change the flight level (compared to the one requested by the aircraft). This maneuver is to be considered as a last resort as it involves an increase in the fuel consumption.

- The probability of acceptance: let $s$ be the current solution with $E(s)$ its energy value and let $s'$ be a neighboring solution of $s$ with $E(s')$ its energy value. The acceptance probability of solution $s'$ is given by $e^{(E(s)−E(s'))/T}$, where $T$ is the temperature.
- The temperature decreases via a geometrical law given by $T_i = \alpha \cdot T_{i-1}$.
- The process stops when the temperature $T$ goes below a predefined final temperature, namely $T_f$. $T_f$ is adjusted to be: $T_f = \beta \cdot T_0$.

1) Objective function: Our goal is to generate a set of $N$ eastbound flights optimal trajectories while satisfying several constraints. There are different route optimality criteria such as total trajectories length, flights duration or fuel consumption. In this study, we choose to minimize the total trajectory duration since it is directly related to fuel consumption. Besides, although we have relaxed several flight parameters, our proposed solution must stay as close as possible to airlines preferences. Thus, we add the total delay and the deviation from the desired rail cost to the objective function. The objective function is then the sum of the three following criteria:

- $C$ : Total cruise time
- $D$ : Total entry delay
- $R$ : Total delay induced by the deviation from the requested track.

Cruising time for each flight is the time needed to fly the sum of distance between the crossing waypoints. Thus, total cruise time, $C$, corresponds to the sum of cruising times over all flights. Total entry delay, $D$, is calculated in minutes. It represents the sum of entry delays over all flights. The deviation delay related to each flight represents required additional time to deviate from the desired track and reach the new assigned one. We get total deviation delay, $R$, by summing up deviation delays related to all flights. The objective function, that we aim to minimize, is the weighted sum of these values as depicted in:

$$F_{obj} = d \cdot D + c \cdot C + r \cdot R$$

where the non-negative coefficients $(d,c,r)$ are used to balance the three criteria up on the user preferences. By minimizing such an objective function, we may obtain a set of optimal trajectories however a conflict-free solution may not exist. For that reason, we have to add the number of induced conflicts to the objective function as the most important criterion to minimize. Actually, we aim to reduce conflicts number to be equal to zero. The objective function becomes then:

$$F_{obj} = C_t + a \cdot (d \cdot D + c \cdot C + r \cdot R)$$

where the coefficient $(a)$ is added in order to give the highest priority to the conflict-free criterion. Once all conflicts are resolved, the system starts to minimize the other criteria (cruising time, deviations and delays) while ensuring that the considered solution remain conflict-free.

VII. RESULTS

In this section, we present our experimental settings and computational results in order to validate our proposed methodology that aim to optimize the strategic eastbound flight planning over NAT airspace. As mentioned earlier, due to the lack of surveillance means, air traffic controllers prefer to keep aircraft in the same track for the entire oceanic route. Since controllers deny re-routing inside the OTS structure, flights exit this structure far from their destinations. This implies the appearance of a very congested zone with a big number of conflicts downstream OTS structure. In order to alleviate the workload of continental controllers, we favor the re-routing of flights inside our proposed route structure so that they exit as close as possible from their destinations. Thus, in the real traffic data we practically find the same entry and exit track for each flight. However, in our simulation tests, we keep the real flight plan, namely: real velocities, entry/exit flight level, entry time and entry track. Then, we generate randomly new exit tracks in order to simulate exit points close to the real aircraft destinations.
A. Example of a conflict resolution

In this section, we consider a simplistic situation between three aircraft in conflict. Then, we illustrate the maneuver of resolution held by our algorithm. As illustrated in figure 7, we consider three aircraft A1, A2 and A3 with respectively their entry time 05:31, 05:41 and 05:45. The vertical flight profile of the three considered aircraft is presented in figure 8. We can clearly notice that A1, A2 and A3 fly at the same flight level, namely FL5, in the entry filter section of the route structure. Then, A2 and A3 begin their climb maneuver us given by their optimal vertical flight profile at the parallel section. However, A1 keep the same Flight level for the entire trajectory. Thus, these climb maneuver explain the occurrence of conflict between A1 and A3 in the entry filter section and between A1 and A2 in the exit filter section.

To resolve these conflicts, our algorithm proposes to change the trajectory of the three aircraft inside the route structure as shown in figure 9. The vertical profile as well as the entry and exit desired tracks have not been changed for the three flights. Nevertheless, the aircraft A1 has been brought forward by 5 minutes. In other more complicated situations, when the algorithm does not find a conflict-free configuration, it opts for changing the desired vertical flight profile. In this case, the modification have to keep the new vertical flight profile as close as possible from the desired one. As described in section IV, the vertical flight profile is represented by an array of 0 and 1 as follow: 0 if the aircraft continue in the same flight level and 1 when the aircraft climbs to the upper flight level (Figure 10-a). Thus, when modifying a desired vertical profile, it is required either to delay or brought forward only one step climb. Let’s consider the example of aircraft A1, if it is necessary to change its desired vertical profile we have only two possibilities of change. These possibilities are presented in figure 10-b and 10-c. The choice between the two assigned vertical flight profile is randomly made.

B. Simulation results without considering the wind network

First, we perform simulations on two real traffic days over the NAT airspace (3rd and 4th August, 2006). Each flight set contains respectively 331 and 378 flights. For these simulations, The parameter values addressed to specify the optimization problem are as follows:

- The initial temperature $T_0 = 0,01$
- The objective function coefficients $a = 0,5$ and $d = c = r = 1$.
- Number of iteration in each temperature schedule $N = 500$.
- The ratio of the temperature decreasing $\alpha = 0,95$,
- The stopping criterion $\beta = 0,0001$,
- The sliding window parameters in minutes: $T_w = 120$, $T_s = 30$.

Actually, the parameters of the SA and SW algorithm are empirically set. On the other side, we adjust the objective function parameters in order to give more priority to the reduction of the number of conflicts, thus we set $a = 0,5$. Besides, we give equal priorities to the other different criterion, namely total cruise time, total delay and total track shift. Hence, we set $d = c = r = 1$. The simulation results for both studied flight sets are presented in table I.

<table>
<thead>
<tr>
<th>Test</th>
<th>03/08/2006</th>
<th>04/08/2006</th>
</tr>
</thead>
<tbody>
<tr>
<td>Number of flights</td>
<td>331</td>
<td>378</td>
</tr>
<tr>
<td>Number of conflicts Before</td>
<td>1055</td>
<td>1548</td>
</tr>
<tr>
<td>After</td>
<td>0</td>
<td>1</td>
</tr>
<tr>
<td>CPU Time (minutes)</td>
<td>43</td>
<td>50</td>
</tr>
<tr>
<td>Number of flights changing their vertical profile</td>
<td>69</td>
<td>78</td>
</tr>
</tbody>
</table>
As we can see in Table I, we conclude that the SA and SW algorithm found almost conflict-free solutions for the two studied flight sets with a reasonable CPU time which is about 50 minutes. Concerning the second flight set (4th August), we denote that 1 residual conflict is unsolved. This remaining conflict can be solved by setting the parameter $a$ of the objective function to 0.1. Thus, we give a bigger priority to conflict number reduction rather than the other criteria. Furthermore, we evaluate the number of flights that changes their vertical profile. In each flight set, typically 70 flight changes their optimal step climbs, thus the rest of the flight set keeps the vertical profile that ensures an optimal fuel consumption. Besides, we evaluate the delay induced for the conflict-free solution. We notice that about 300 flight in each set are within 10 minutes of delay and only some flights are approaching the limit delay which is 20 minutes. These encouraging results allowed us to expend the flight number and re-experiment the simulations. Thus, we generate randomly a flight set containing 1000 flights. Initially, the considered flight set generates 5501 conflicts. After applying SA and SW algorithm, we noticed a significant number reduction that reaches 119 conflicts. However, a conflict-free solution does not exist with the previously mentioned configuration of the SA algorithm. For this reason, we tested our problem with different SA algorithm configurations. Table II summarizes the obtained results. We notice that the number of remaining conflict, as well as the number of flights that changes their requested vertical profile, are strongly affected by the changing of both parameters $\alpha$ and $N$. Slowly lowering the temperature, by decreasing the parameter $\alpha$, is influencing more the results. Though, more CPU time is needed to get an optimal solution. Nevertheless, although the search space is further explored by increasing the parameters $\alpha$ and $N$, no conflict free solution is found. Conflict number decreases from 5501 to 32. This is considered, in our case, as a very interesting result. In fact, we are tackling a strategic conflict resolution, and therefore, any remaining conflicts could be resolved in pre-tactical and tactical phases.

### C. Simulation results considering the wind network

In this section, we re-evaluate the results while applying an experimental wind network. Since the results for different flight sets are nearly similar, we focus only on the traffic day 4th August 2006. Actually, when we apply a wind field to the conflict-free solution found in the aforementioned section, we notice that a number of new conflicts reappear. This result is reasonable and proves the importance of wind impact in the flight's progress. Thus, it is necessary to perform simulations considering the wind information. To prove the efficiency of our new route structure under wind, we compute the time saving for each flight trajectory when considering an empirical wind field. Time savings statistics show that a significant gain in traveling time is reached. It ranges between 1 and 21 minutes for each individual flight. Besides, the average time savings for the considered flight set is found to be 6.5 minutes.
REFERENCES


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